US-CL-CURRENT: 264/51,264/55

US-PAT-NO: 4806293

DOCUMENT-IDENTIFIER: US 4806293 A

TITLE: Method of producing a foamed, molded article

DATE-ISSUED: February 21, 1989

INVENTOR-INFORMATION:

NAME	CITY	STATE	ZIP CODE
COUNTRY Akiyama; Hiroyuki JPX	Hiratsuka	N/A	N/A
Sudo; Yoshimi	Chigasaki	N/A	N/A
JPX Kishida; Masahiko JPX	Hiratsuka	N/A	N/A
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US-CL-CURRENT: 264/53,264/51 ,264/55

ABSTRACT:

Method of producing a molded article of a foamed thermoplastic

molten mass of an expandable thermoplastic resin is accumulated

accumulator while it is prevented from foaming. A predetermined quantity of

the accumulated thermoplastic resin is ejected rapidly from the accumulator

into the atmosphere so that the thermoplastic resin commences foaming.

ejected thermoplastic resin is placed in a mold cavity before the

expansion has been completed and is compressed. The expansion and molding of

the ejected thermoplastic resin is completed in the mold while controlling the

compression pressure to obtain a foamed molded article.

5 Claims, 13 Drawing figures Exemplary Claim Number:

Number of Drawing Sheets:

In the present invention, it is preferred that the molten resin 10 discharged

from the accumulator 5 exhibit a low expansion speed. of the melt

index (MI) value of the resin, the kind and amount of the blowing agent, the

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kind and amount of the expansion aid (cell adjusting agent) and the shape and

size of the cross-section of the die 7 of the accumulator 5 through which the $\,$

resin is discharged have an influence upon the expansion speed. It is

especially effective to select a die having such a size and a shape that can

provide only a small difference in pressure between the atmosphere into which

the molten resin is discharged therethrough and the inside of the ${\it accumulator}$

from which the discharge of the molten resin has just been completed. It is

also effective to minimize the amount of the expansion aid. For example, in

the case of high density polyethylenes having an MI value of 0.5-20, the use of

5-20 parts by weight of dichlorotetrafluoroethane and/or dichlorodifluoromethane, or 0-0.05 part by weight of talc per 100 parts by

weight of the polyethylene is recommended.

4762860

US-CL-CURRENT: 521/134,521/136 ,521/139 ,521/143 ,521/146 ,521/154 ,521/89 ,521/93

US-PAT-NO: 4762860

DOCUMENT-IDENTIFIER: US 4762860 A

TITLE: Alcohol control of lightly crosslinked foamed polymer

production

DATE-ISSUED: August 9, 1988

INVENTOR-INFORMATION:

NAME CITY STATE ZIP CODE

COUNTRY

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N/A

US-CL-CURRENT: 521/88,521/134 ,521/136 ,521/139 ,521/143 ,521/146

,521/154

,521/89 ,521/93

ABSTRACT:

An expandable ethylenic or styrenic polymer composition for production of

lightly crosslinked foamed polymers and a process for controlling the degree of

crosslinking of the polymer prior to extrusion foaming. The control is

obtained by use of (a) a reversible gas-yielding crosslinking reaction which is

delayed in the foam extrusion line in the presence of gaseous products

(alcohols) and (b) added amounts of an alcohol such as an aliphatic alcohol.

Suitable crosslinking agents include silanes, azido functional silanes,

titanates, and amino compounds.

5 Claims, 0 Drawing figures

Exemplary Claim Number:

DEPR:

In this example, the same apparatus as in Example I was used. A high density $\ensuremath{\mathsf{I}}$

polyethylene (HDPE) having 0.6 melt index (ASTM D-1238-79

Condition E) and

 $0.963~\mathrm{g/cc}$ density was used in this example. The polymer granules were mixed

with 0.05 pph talc and 0.05 pph organotin catalyst (T-12). The mixture was fed

into the extruder at 10 pounds per hour. Extruder zones were maintained at

160.degree., 200.degree. and 200.degree. C. for feeding, melting and metering, and mixing zone, respectively. The gel temperaure was maintained at about 130.degree. C. and a 90/10 mixture of FC-12/EtOH was used as the blowing agent. The test results are presented in Table G.

DETL: TABLE D

BLOWING AGENT TYPE TALC HMMM DIE DIE EXTR. FOAM TEST LEVEL (pph) LEVEL LEVEL GAP PRES. PRES. THICK. NO. (12) (1) (13) (2) (3) (4) (5) (6)

1
FC-12 20.3 0.3 -- 0.18 430 1210 1.44 2 FC-12 21.6 0.3 0.2
0.18 600 1720
1.42 3 FC-12/EtOH:80/20 18.8 0.4 -- 0.13 380 890 1.23 4
FC-12/EtOH:80/20
18.8 0.4 0.7 0.13 435 980 1.24 5 FC-114/MeOH:90/10 24.3 0.6
-- 0.10 405
1040 0.89 6 FC-114/MeOH:90/10 24.4 0.6 1.5 0.10 455 1210
0.79

FOAM
FOAM CELL PREFOAMING COLLAPSE RESISTANCE TEST WIDTH DENS.
SIZE (?) 95
100 105 110 115.degree. C. NO. (7) (8) (9) (10) (11)

1.51 1.61 1.01 verge 96 87 31 30 ND 2 1.60 2.18 1.62 melt fract 88 80 26
13 ND 3 1.45 1.97 1.25 no 100 97 56 40 29 4 1.64 1.89 1.25 no 99 98 85
71 62 5 1.36 1.61 1.01 no 95 89 17 13 ND 6 1.35 1.76 1.08 no 93 82 49 31

ND = not determined (1) parts of blowing agent mixed in per hundred parts of polymer (2) through (11) = the same as in Table B (12) FC12 = dichlorofluoromethane, FC114 = dichlorotetrafluoroethane, EtO = ethanol, MeOH = methanol (13) parts of talcum powder mixed in per hundred parts of polymer

4,847,150

US-CL-CURRENT: 264/53,264/DIG.18 ,264/DIG.5 ,521/134 ,521/139 ,521/140 ,521/143 ,521/146 ,521/149 ,521/79 ,521/81 ,521/96 ,525/22 ,525/80 ,525/96 ,525/98

US-PAT-NO: 4847150

DOCUMENT-IDENTIFIER: US 4847150 A

TITLE: Foams of polyolefin/polystyrene resin mixture

DATE-ISSUED: July 11, 1989

INVENTOR-INFORMATION:

NAME CITY STATE

COUNTRY

Takeda; Noboru Suzuki N/A N/A

JPX

US-CL-CURRENT: 428/318.8,264/53 ,264/DIG.18 ,264/DIG.5 ,521/134 ,521/139

ZIP CODE

,521/140 ,521/143 ,521/146 ,521/149 ,521/79 ,521/81 ,521/96

,525/222 ,525/80

,525/96 ,525/98

ABSTRACT:

A foam of a polyolefin/polystyrene resin mixture obtained by mixing a

polyolefin resin and a polystyrene resin in the presence of a hydrogenated

styrene/butadiene block copolyer, and subjecting the resultant mixed resinous

composition to extrusion foaming, wherein;

- (1) said hydrogenated styrene/butadiene block copolymer comprises, as components before hydrogenation, 10 to 38% by weight of styrene and butadiene with a content of 1,2-bond type butadiene of 20 to 50% by weight based on butadiene, and;
- (2) said foam comprises a thin surface skin portion showing a value of 0.65 or more of the surface structural index S represented by the following formula:

S=t/T.gtoreq.0.65

wherein t and T each represent a total light-transmission evaluated according to the method of ASTM D1003 with respect to a surface skin layer and

an inner layer of the foam,

is found to have the cushioning properties (or the foam properties) that enables elastic cushioning of a large load. 1 Claims, 18 Drawing figures Exemplary Claim Number: Number of Drawing Sheets:

DEPR: To a mixture of (52% by weight) of high density polyethylene (produced by Asahi Kasei K.K.; B870; M.I.=0.3; density: 0.960 g/cc), 35% by weight of polystyrene (produced by Asahi Kasei K.K.; Stylon 605; M.F.R.=1.5) and 13% by weight of a hydrogenated styrene/butadiene block copolymer A, 0.1% by weight of talc was added as a nucleating. The resultant mixture was dryblended in a Henschel mixer and then thoroughly kneaded in a kneading extruder to obtain a resin mixture as a base material. The base material mixture obtained continuously fed to an extruder having a bore of 65 mm at the rate of 60 kg/hr to carry out melt kneading, and also, from an inlet for a blowing agent

provided at a tip end of the extruder, a blowing agent mixture composed of

dichlorotetrafluoroethane and methylene chloride in molar ratio of 7:3 was

continuously introduced under pressure and at the rate of 21.7 kg/hr to carry

out melt kneading at high temperature and under high pressure. Thereafter, the

resultant melt was cooled to 128.degree. C. in a cooling device, and extruded

through a die comprising a slit of 2.8 mmt.times.50 mmW, a land of 4 mmL and a

taper angle of 30.degree. to a zone of atmospheric pressure to effect

expanding. Shear stress (.DELTA.P.times.t/2L) at the land portion was found to

be 3.2 kg/cm.sup.2. There was obtained a foam having a density of 20

kg/m.sup.3 and an average cell diameter of 1.0 mm, which was homogeneous and of

high commercial value. The index S showing the surface structure was 0.83.

12/26/2001, EAST Version: 1.02.0008

Results obtained by evaluations made in accordance with the methods as described above are shown in Table 4.

DEPR:

Low density polyethylene (produced by Asahi Kasei K.K.; F-1920; M.I.=2.0;

density: 0.919 g/cc) and 0.4 part by weight of talc as a nucleating agent were

continuously fed to an extruder having a bore of 65 mm to carry out melt

kneading. From an inlet for a blowing agent provided at a tip end of the

extruder, dichlorotetrafluoroethane in amount of 14 parts by weight based on

100 parts by weight of the base material resin was introduced under pressure to

carry out melt kneading at high temperature and under high pressure.

Thereafter, the resultant melt was cooled to 106.degree. C. in a cooling

device, and extruded through a die to a zone of atmospheric pressure to effect

expanding. There was obtained a foam having a density of 50 kg/m.sup.3, an

average cell diameter of 1.0 mm and a closed-cell percentage of 100%.

DEPR:

60% by weight of low density polyethylene (produced by Asahi Kasei K.K.; Q902;

M.I.=0.3; density: 0.920/cc), 40% by weight of polystyrene (produced by Asahi

Kasei K.K.; Stylon 680; M.F.R.=7.5) and 0.1 part by weight of talc as a cell

controlling agent were continuously fed to an extruder having a bore of 65~mm,

followed by carrying out the same operations as in Example 1 to produce a foam.

The foam thus obtained had a density of 25 kg/m.sup.3, an average cell diameter

of 1.0 mm and a closed-cell percentage of 100%. For reference, the index ${\sf S}$

showing the surface structure was found to be 0.52.

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